

## Rods with intrinsic curvature

$$\textcircled{1} E = \int_0^L d\xi \left( \frac{1}{2} EI_1 (v_1 - v_{10})^2 + \frac{1}{2} EI_2 (v_2 - v_{20})^2 + \frac{1}{2} \mu J (v_3 - v_{30})^2 \right).$$

$\xi$ : arc length

$$\Rightarrow \begin{cases} p(\xi) + n'(\xi) = 0 \\ m'(\xi) + r'(\xi) \times n(\xi) + q(\xi) = 0 \end{cases} \quad \text{where}$$

$$m = (EI_1 (v_1 - v_{10}), EI_2 (v_2 - v_{20}), \mu J (v_3 - v_{30}))$$

in  $\{d_1, d_2, d_3\}$  basis

$$\textcircled{2} \{E_1, E_2, E_3\}, \{D_1, D_2, D_3\}, \{d_1, d_2, d_3\}$$

$$\cancel{d\alpha = PP_0 E} \quad \begin{pmatrix} d_1 \\ d_2 \\ d_3 \end{pmatrix} = PP_0 \begin{pmatrix} E_1 \\ E_2 \\ E_3 \end{pmatrix}$$

$P_0$  is known from the reference configuration.

$$\textcircled{3} \text{ Solving the ODE system in } \textcircled{1}, \text{ we obtain } v_k - v_{k0}(\xi)$$

$$\textcircled{4} \text{ Euler angles } P = Q(\alpha_3, \hat{e}_3) Q(\alpha_2, \hat{e}_2) Q(\alpha_1, \hat{e}_1)$$

$$\textcircled{5} \alpha_1 = \alpha_{10}, \alpha_2 = \alpha_{20}, \alpha_3 = \alpha_{30} \quad \text{initial condition.}$$

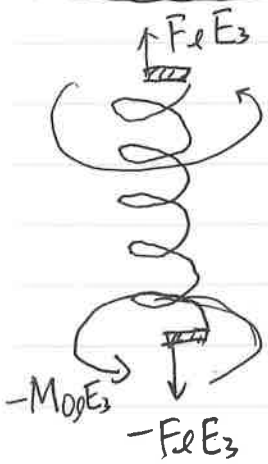
$$\begin{pmatrix} \frac{\partial \alpha_1}{\partial \xi} \\ \frac{\partial \alpha_2}{\partial \xi} \\ \frac{\partial \alpha_3}{\partial \xi} \end{pmatrix} = \begin{pmatrix} -\cos \alpha_2 \cos \alpha_3 & \cos \alpha_2 \sin \alpha_3 & 0 \\ \sin \alpha_3 & \cos \alpha_3 & 0 \\ \cot \alpha_2 \cos \alpha_3 & -\cot \alpha_2 \sin \alpha_3 & 1 \end{pmatrix} \begin{pmatrix} v_1 \\ v_2 \\ v_3 \end{pmatrix}$$

$$\Rightarrow \alpha_1(\xi), \alpha_2(\xi), \alpha_3(\xi)$$

$$\textcircled{6} d\alpha' = (P(v + v_0)) \times d\alpha$$

$$\textcircled{7} r'(\xi) = d_3(\xi) \Rightarrow r = \int_0^\xi d_3(\xi) d\xi + d_3(0)$$

### Example: spiral springs



$$\vec{M}_e = M_e e_3 = M_e + r(l) \times F_e$$

- $e_n$  is in the plane of  $E_1, E_2$
- In principle,  $\{D_1, D_2, D_3\}$  can be chosen arbitrarily. However, it is convenient to choose  $\{D_1, D_2, D_3\} = \{e_n, e_t, e_3\}$ , where  $\{e_t, e_n, e_3\}$  is the Frenet frame.

$$P_0 = Q(\varphi_2, \cos \varphi_1 E_1 + \sin \varphi_1 E_2) Q(\varphi_1, E_3)$$

$$e_n = \cos \varphi_1 E_1 + \sin \varphi_1 E_2$$

Following the previous discussion:

② Compute  $P_0$ : — Mathematica.

$$\text{Compute } v_0: v_0 = \text{ax}(P_0 P_0^T) = v_{10} D_1 + v_{20} D_2 + v_{30} D_3$$

$$= \varphi_1' \sin \varphi_2 D_2 + \varphi_1' \cos \varphi_2 D_3$$

• If the spring:  $R(s) = R e_{00} + R \theta_0(s) \tan(\zeta) E_3$

$$e_{00} = \cos(\theta_0(s)) E_1 + \sin(\theta_0(s)) E_2$$

$$\Rightarrow \theta_0(s) = \varphi_1(s) - \pi, \quad \zeta = \frac{\pi}{2} - \varphi_2(s) \Rightarrow \varphi_2'(s) = 0!$$

③ Balance law.

$$\begin{cases} n' = 0 \\ m' + r' \times n = 0 \end{cases} \quad m = EI_1 v_1 d_1 + EI_2 v_2 d_2 + \mu J v_3 d_3$$

$$n' = 0 \Rightarrow n = \text{const.} = F_0 = F_{01} d_1 + F_{02} d_2 + F_{03} d_3$$

$$dk' = \left( \sum_{i=1}^3 (v_i + v_{i0}) d_i \right) \times dk \quad \sim \textcircled{6}$$

$$\begin{aligned}
 m' = & EI_1 v_1' d_1 + EI_2 v_2' d_2 + \mu J v_3' d_3 \\
 & + EI_1 v_1 [-(v_2 + v_{20}) d_3 + (v_3 + v_{30}) d_2] \\
 & + EI_2 v_2 [(v_1 + v_{10}) d_3 - (v_3 + v_{30}) d_1] \\
 & + \mu J v_3 [-(v_1 + v_{10}) d_2 + (v_2 + v_{20}) d_1]
 \end{aligned}$$

$$\Rightarrow \begin{cases} EI_1 v_1' - EI_2 v_2 (v_3 + v_{30}) + \mu J v_3 (v_2 + v_{20}) = +F_{02} \\ EI_2 v_2' - \mu J (v_1 + v_{10}) v_3 + EI_1 (v_3 + v_{30}) v_1 = -F_{01} \\ \mu J v_3' - EI_1 (v_2 + v_{20}) v_1 + EI_2 (v_1 + v_{10}) v_2 = 0 \end{cases}$$

③ For our springs problem:  $I_1 = I_2 = I$

$$BC_s: n(l^-) = F_0 E_3, \quad m(l^-) = M_{02} E_3 - r(l^-) \times F_0 E_3$$

$$\text{strain: } v_{00} = 0, \quad v_{02} = \varphi_1' \sin \varphi_2, \quad v_{03} = \varphi_1' \cos \varphi_2$$

$$\Rightarrow \begin{cases} EI v_1' - EI v_2 (v_3 + v_{03}) + \mu J (v_2 + v_{02}) v_3 = d_2 \cdot F_0 E_3 \\ EI v_2' - \mu J v_1 v_3 + EI (v_3 + v_{03}) v_1 = -d_1 \cdot F_0 E_3 \\ \mu J v_3' - EI v_{02} v_1 = 0 \end{cases} \quad *$$

We seek the boundary conditions  $F_0$  and  $M_{02}$  that will deform  $R(s)$  to

$$r(s) = r (\cos \theta(s) E_1 + \sin \theta(s) E_2) + r \theta(s) \tan \alpha E_3$$

$$\boxed{\text{Assumption: } \tilde{e}_t = d_3, \quad \tilde{e}_n = d_1, \quad \tilde{e}_b = d_2}$$

$$PR = Q \left( \frac{\pi}{2} - \alpha, \cos(\theta + \pi) E_1 + \sin(\theta + \pi) E_2 \right) Q(\theta + \pi, E_3)$$

$$\Rightarrow P = PR_0 \cdot P_0^{-1} \quad (\text{see Mathe matica})$$

$$\Rightarrow v_1=0, \quad v_2=k-k_0, \quad v_3=\tau-\tau_0 \quad \text{in } \{D_1, D_2, D_3\}$$

$$\text{where } k = \frac{\cos^2 \sigma}{r}, \quad \tau = \frac{\cos \sigma \sin \sigma}{r}, \quad k_0 = \frac{\cos^2 \xi}{R}, \quad \tau_0 = \frac{\cos \xi \sin \xi}{R}$$

$$\star \Rightarrow \begin{cases} d_1 \cdot F_d E_3 = 0, \quad v_1 = 0 & (\text{substitute } v_1' = v_2' = v_3' = 0) \\ EI v_2 (v_3 + v_{03}) - \mu J (v_2 + v_{02}) v_3 + d_2 \cdot F_d E_3 = 0 \end{cases}$$

$$\Rightarrow \cos \sigma F_d = \mu J k (\tau - \tau_0) - EI \tau (k - k_0) \quad \sim (1)$$

$$\vec{m} = EI (k - k_0) d_2 + \mu J (\tau - \tau_0) d_3$$

$$\Rightarrow M_{02} = EI (k - k_0) \cos \sigma + \mu J (\tau - \tau_0) \sin \sigma \quad \sim (2)$$

(1) and (2) are the BCs that deform  $R(s)$  into  $k(s)$ .  $\square$